

EXCM calculations

Notice regarding the use of the H-type EXCM/EXCH gantry without motion PLC.

This application note explain how to calculate the dynamics data for each motors to obtain a linear movement in the 2D cartesian system.

EXCM
EXCH

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1 Components





Photo	Type/Name	Part n°	Links
	EXCM-30-	2226101	  

Table 1.1: Components/Software used

2 Introduction

2.1 Hardware Configuration

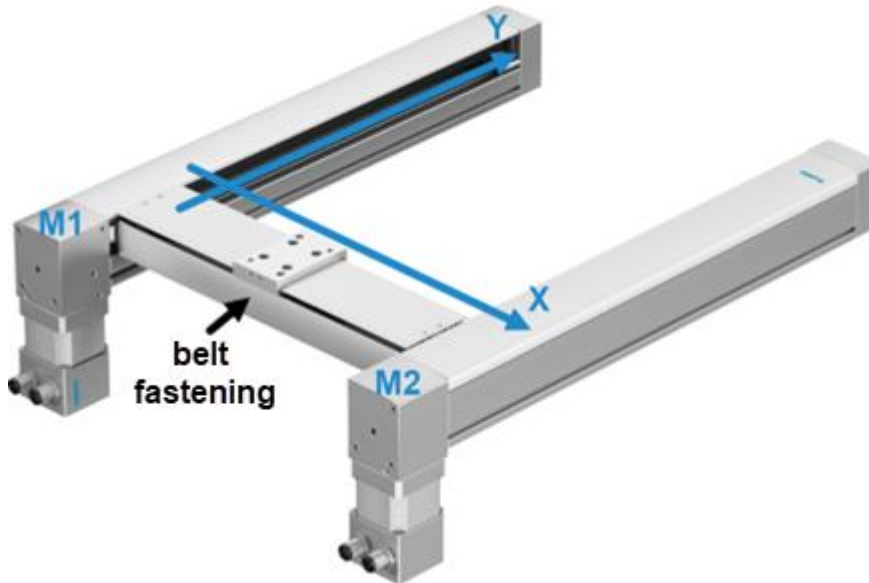


Fig. 2.1: EXCM-30

2.2 Conversion Matrices













To know the angular positions θ_1 and θ_2 (rad) of each motor from the Cartesian position $[X;Y]$ (mm)

$$\begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} = \frac{1}{radius} * \begin{bmatrix} -1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \end{bmatrix}$$

To determine the cartesian position $[X;Y]$ from the angular positions θ_1 and θ_2 (rad)

$$\begin{bmatrix} X \\ Y \end{bmatrix} = \frac{radius}{2} * \begin{bmatrix} -1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

The motor controllers are each configured with their own motor and the unit of measurement is the radian (rad; rad/s; rad/s²)

 Servo drive	CMMT-ST-C8-1C-EC-S0 8084005 Licenses	Maximum Current 10,00 A	Intermediate Circuit Voltage 48,00 V	Supply Voltage 24,00 V	 			
 Motor	EMMS-ST-42-S-SE-S1-G3 2253453	Type Stepper motor (1)	Holding Brake No	Encoder Protocol Incremental (4)	Encoder Type None (0)	Voltage 48,00 V	Virtual Mode Deactivated	 
 Axis	User defined rotative axis	Position Range Unlimited	 					
 Mounting Kit	User Defined Mounting Kit	Type Axial	Gear Ratio 1:1	 				

Introduction

The use of radians is not mandatory, it is quite possible to change the unit of measurement and adapt the matrices accordingly.

For example in rev turns [r, r/s, r/s² ...]

	EMMS-ST-42-S-SE-S1-G3 2253453	Type Stepper motor (1)	Holding Br No
	User defined rotative axis	Position Range Unlimited	
	User Defined Mounting Kit	Type Axial	Gear Ratio 1:1
	No gear configured		

Select Axis

User defined rotative axis

Actual user unit: Rev [r, r/s, ...] (2)

Motion: Rotative

Unlimited axis: Active

Design axis: Single axis (0)

$$\begin{bmatrix} \theta 1 \\ \theta 2 \end{bmatrix} = \frac{1}{\text{feed constant}} * \begin{bmatrix} -1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \end{bmatrix}$$

$$\begin{bmatrix} X \\ Y \end{bmatrix} = \frac{\text{feed constant}}{2} * \begin{bmatrix} -1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} \theta 1 \\ \theta 2 \end{bmatrix}$$

The feed constant per revolution of an EXCM-30 is 38mm/revolution.

If we apply the matrix to know the cartesian position, this gives 2 equations:

$$\theta 1 = PosMot1$$

$$\theta 2 = PosMot2$$

$$X = \frac{38}{2} * (-PosMot1 - PosMot2)$$

$$Y = \frac{38}{2} * (-PosMot1 + PosMot2)$$

3 Trajectory management

With these conversions it is then possible to send Cartesian instructions [X,Y], but the movement will not be rectilinear, and we will obtain a displacement similar to the red trajectory.

To obtain a straight displacement (green trajectory), it is necessary to determine the dynamics of each motor so that their travel time is equal.

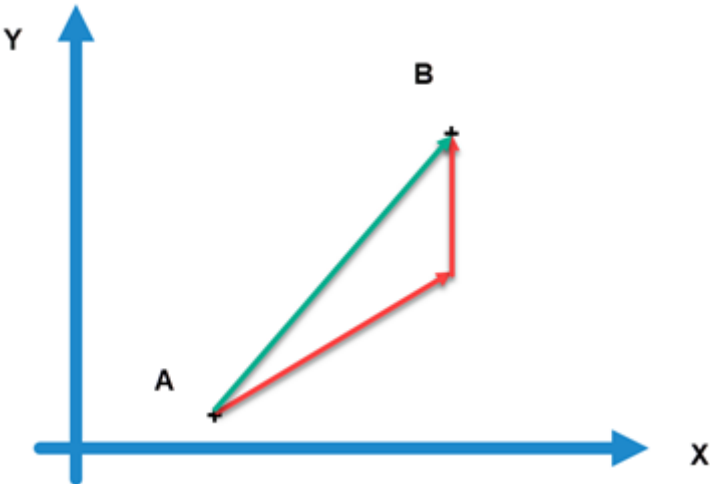


Fig. 3.1: Trajectories of Movements

Additional equations will be used to calculate the speeds, accelerations and deceleration for each engine

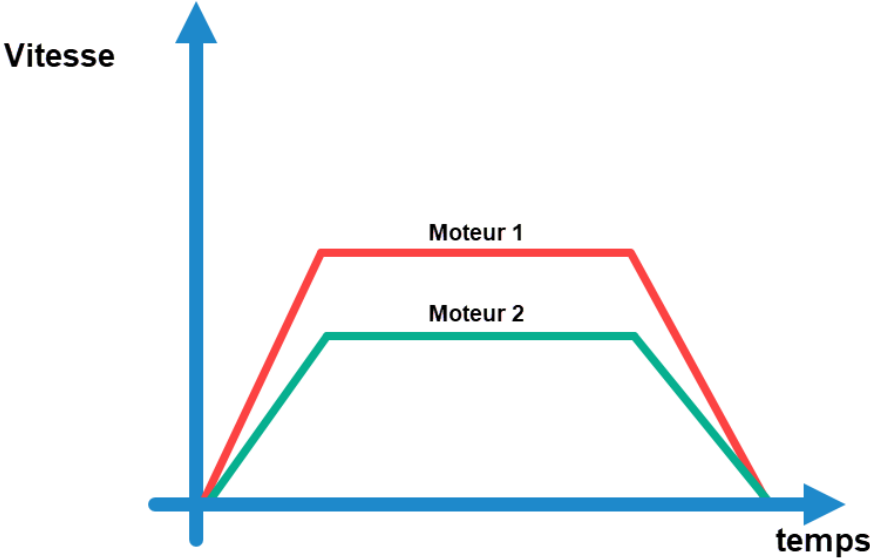


Fig. 3.2: Combined motor speeds

4 Kinematic equations

Starting position	Setpoint	Unknowns to be determined
Angular position M1 (θ_{1A})	Position X_B (mm)	Angular position M1 (θ_{1B})
Angular position M2 (θ_{2A})	Position Y_B (mm)	Angular position M2 (θ_{2B})
Position X_A (mm)	Velocity (mm/s)	Velocity M1
Position Y_A (mm)	Acceleration (mm/s ²)	Velocity M2
	Deceleration (mm/s ²)	Acceleration M1
		Deceleration M1
		Acceleration M2
		Deceleration M2

Table 4.1: Input data

The units of measurement of the unknowns to be determined are based on the parameterization made in the Festo Automation Suite software.

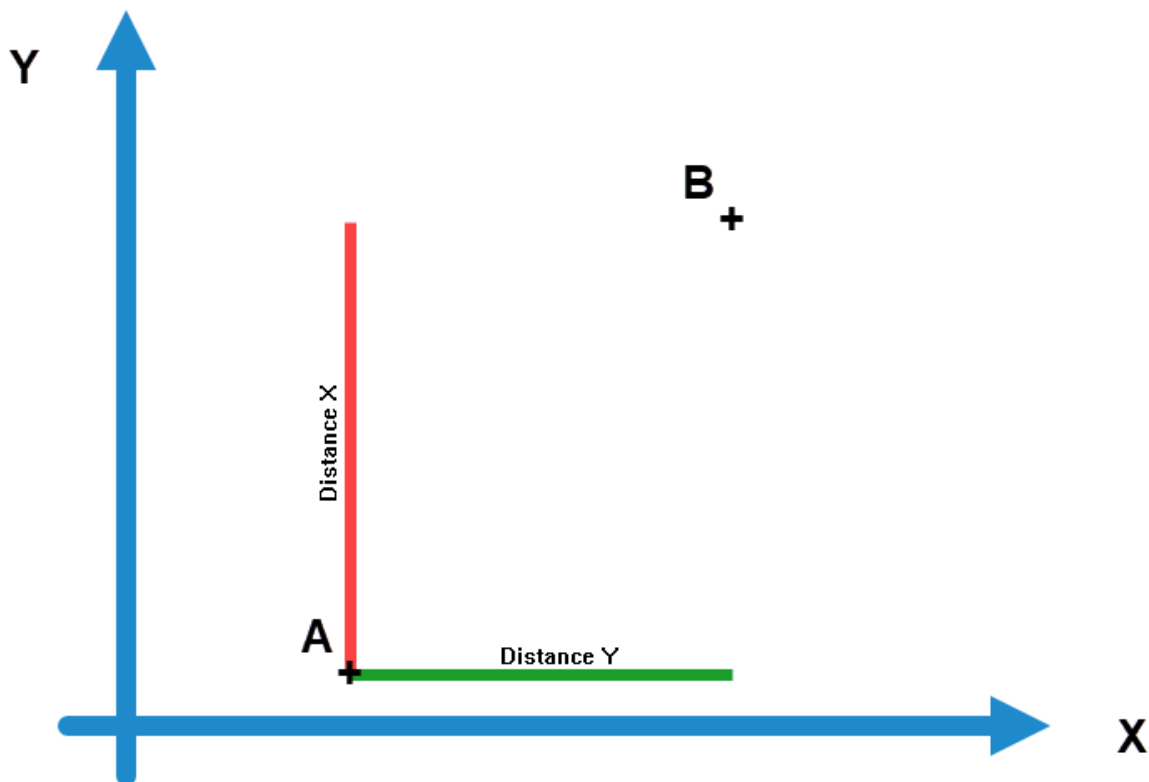
4.1 Calculation of distances by Axis (mm) and motor (rev)

Distance $X_{AB} = \text{actual position } X_A - \text{setpoint } X_B$

Distance $Y_{AB} = \text{actual position } Y_A - \text{setpoint } Y_B$

angular distance M1 = actual position $\theta_{1A} - \text{setpoint } \theta_{1A}$

angular distance M2 = actual position $\theta_{2A} - \text{setpoint } \theta_{2B}$

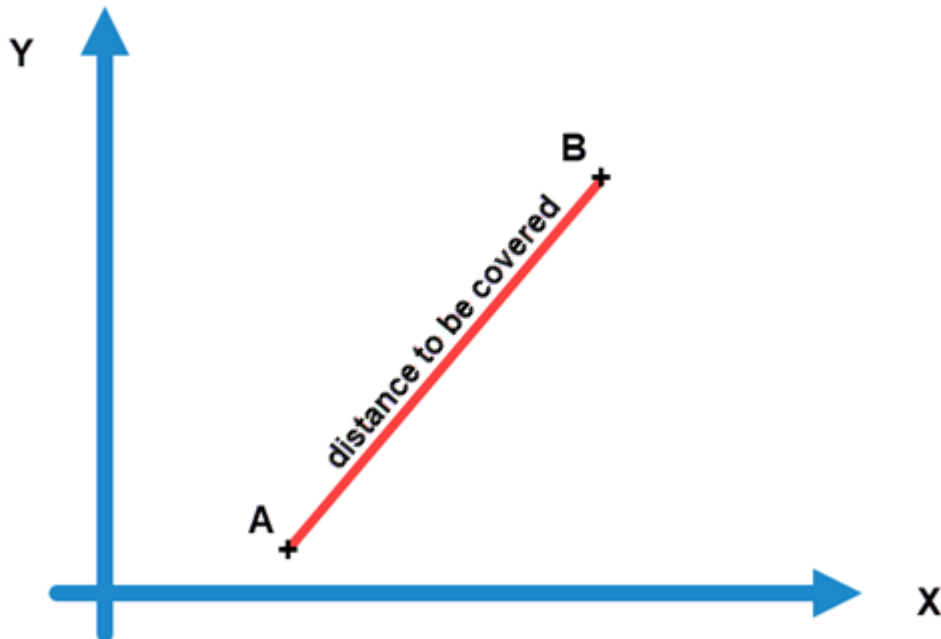


A = current position.

B = position setpoint to be reached.

4.2 Calculation of the distance to be covered [X,Y], (Pythagoras)

$$\text{distance to be covered} = \sqrt{\text{distance on } X^2 + \text{distance on } Y^2}$$



4.3 Calculation of acceleration and deceleration times

$$\text{time}_{acc} = \frac{\text{Velocity}}{\text{acceleration}}$$

$$\text{time}_{dec} = \frac{\text{Velocity}}{\text{deceleration}}$$

4.4 Calculation of acceleration and deceleration distances

$$\text{acc distance} = \frac{1}{2} * \text{acceleration} * \text{time}_{acc}^2$$

$$\text{acc distance} = \frac{1}{2} * \text{deceleration} * \text{time}_{dec}^2$$

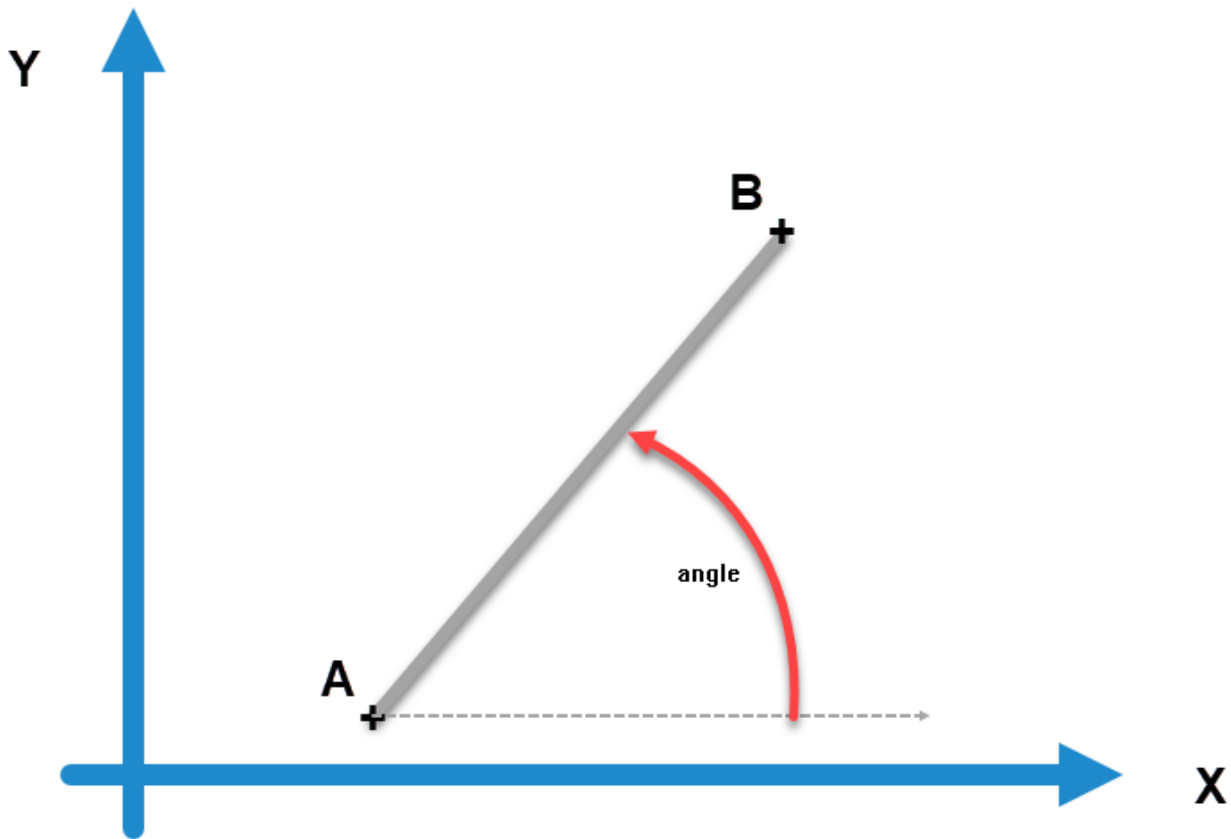
4.5 Calculating the distance traveled at Vmax

$$\text{Vmax distance} = \text{distance to be covered} - (\text{Acc distance} + \text{Dec distance})$$

Optional formula, to determine if the maximum speed can be reached $\text{Vmax distance} > 0$

4.6 Determination of the Direction of Motion Angle

$$\text{angle} = \tan^{-1} * \left(\frac{\text{Distance } Y_{AB}}{\text{Distance } X_{AB}} \right)$$



4.7 X & Y axis projection

α = angle

*Acc distance on X = sin α * Acc distance*

*Dec distance on X = sin α * Dec distance*

*Acc distance on Y = cos α * Acc distance*

*Dec distance on Y = cos α * Dec distance*

4.8 Conversion of Acceleration Distances and Engine Rotation Deceleration

We consider that the parameterized unit is: Rev [r, r/s, r/s² ...] and that the feed constance = 38mm.

$$\text{Acc distance } M1 = \frac{1}{38} * (\text{Acc distance } X + \text{Acc distance } Y)$$

$$\text{Dec distance } M1 = \frac{1}{38} * (\text{Dec distance } X + \text{Dec distance } Y)$$

$$\text{Acc distance } M2 = \frac{1}{38} * (\text{Acc distance } X - \text{Acc distance } Y)$$

$$\text{Dec distance } M2 = \frac{1}{38} * (\text{Dec distance } X - \text{Dec distance } Y)$$

4.9 Determination of Rotational Acceleration and Deceleration/s²

$$\mathbf{Acc\ M1} = 2 * \frac{\mathit{Acc\ distance\ M1}}{\mathit{Acc\ time}^2}$$

$$\mathbf{Dec\ M1} = 2 * \frac{\mathit{Dec\ distance\ M1}}{\mathit{Dec\ time}^2}$$

$$\mathbf{Acc\ M2} = 2 * \frac{\mathit{Acc\ distance\ M2}}{\mathit{Acc\ Time}^2}$$

$$\mathbf{Dec\ M2} = 2 * \frac{\mathit{Dec\ distance\ M2}}{\mathit{Dec\ Time}^2}$$


4.10 Determination of velocity, rev/s

$$\mathbf{M1\ Velocity} = \mathit{M1\ Acc} * \mathit{Acc\ time}$$

$$\mathbf{M2\ Velocity} = \mathit{M2\ Acc} * \mathit{Acc\ time}$$

5 Motion Controls

In this sample, the Festo point to point Library for Codesys3.5 is used, it's available on Festo Support Portal



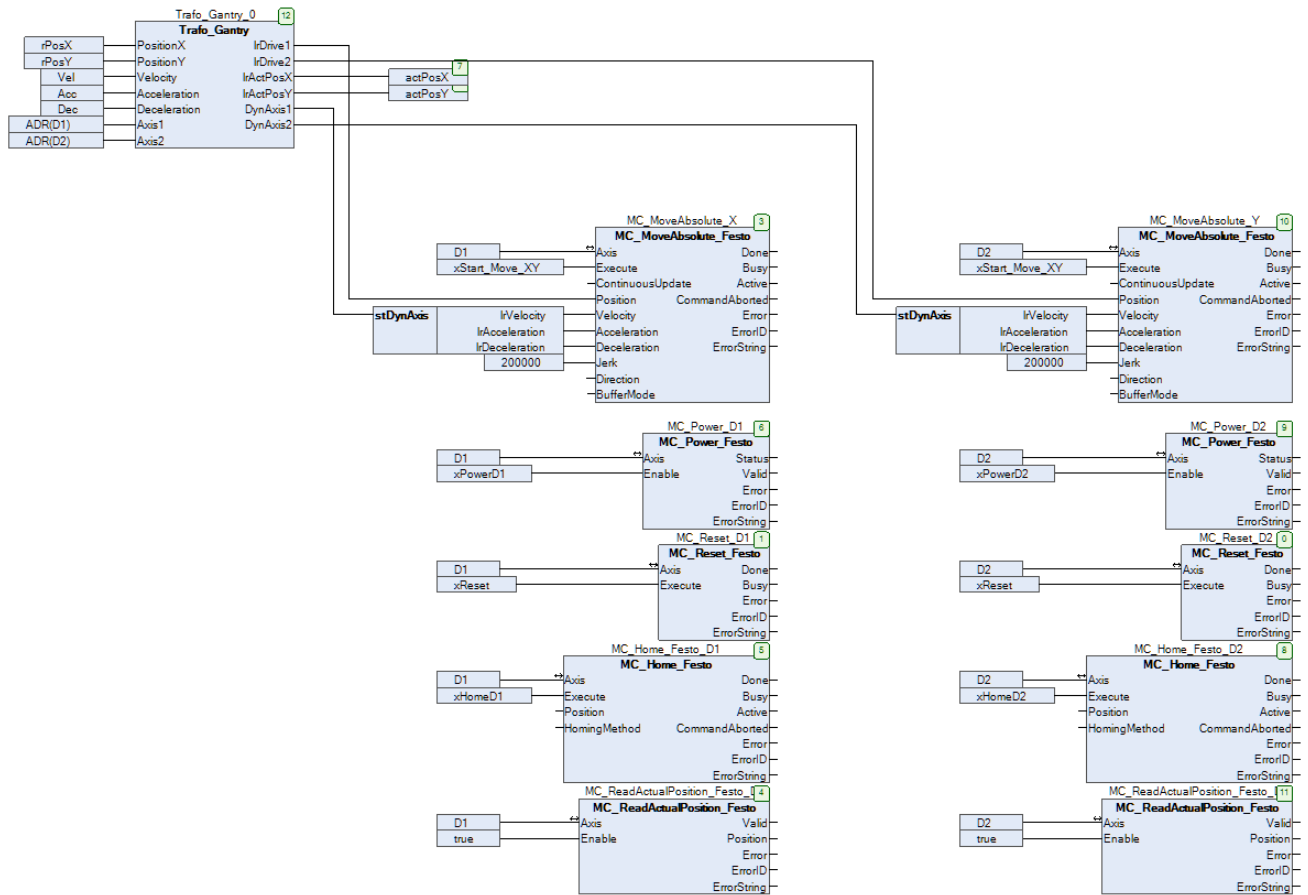
Function blocks CODESYS

PtP function blocks for Codesys 3.5
Point-to-point (PtP) library for servo drives with EtherCAT (CiA402)
in the Codesys V3.5 development environment.

All the calculation are implemented in an function bloc named Trafo_Gantry, the source code is shown at the next page.

Each motor can then be controlled individually and simultaneously by applying the calculated setpoints for each one

Position, Acceleration, Speed and Deceleration.



```

1 // needed for axis Position, could be replaced by MC_ReadActualPosition_Festo
2 D1:=Axis1^;
3 D2:=Axis2^;
4
5 //Hgantry Conversion Matrices
6 lrDrive1:=(1/lrRadius)*((-1*PositionX)+(-1*PositionY));
7 lrDrive2:=(1/lrRadius)*((-1*PositionX)+(1*PositionY));
8
9 lrActPosX:=(lrRadius/2)*((-1*D1.ActualPosition)+(-1*D2.ActualPosition));
10 lrActPosY:=(lrRadius/2)*((-1*D1.ActualPosition)+(1*D2.ActualPosition));
11
12 // Calculation of distances by Axis (mm) and motor (rev)
13 lrDistX:=lrActPosX-PositionX;
14 lrDistY:=lrActPosY-PositionY;
15
16 lrDistD1:=D1.ActualPosition-lrDrive1;
17 lrDistD2:=D2.ActualPosition-lrDrive2;
18
19 // Calculation of the distance to be covered [X,Y], (Pythagoras)
20 lrDistCart:=SQRT(EXPT(lrDistX,2)+EXPT(lrDistY,2));
21
22 // Calculation of acceleration and deceleration times
23 lrTpsAcc:=Velocity/Acceleration;
24 lrTpsDec:=Velocity/Deceleration;
25
26 // Calculation of acceleration and deceleration distances
27 lrDistAcc:=0.5*Acceleration*EXPT(lrTpsAcc,2);
28 lrDistDec:=0.5*Deceleration*EXPT(lrTpsDec,2);
29
30 // Determination of the Direction of Motion Angle
31 lrAngle:=ATAN(lrDistY/lrDistX);
32
33 // X & Y axis projection
34 lrDistAccX:=SIN(lrAngle)*lrDistAcc;
35 lrDistDecX:=SIN(lrAngle)*lrDistDec;
36 lrDistAccY:=COS(lrAngle)*lrDistAcc;
37 lrDistDecY:=COS(lrAngle)*lrDistDec;
38
39 // Conversion of Acceleration Distances and Engine Rotation Deceleration
40 lrDistAccD1:=ABS((1/lrRadius)*((1*lrDistAccX)+(1*lrDistAccY)));
41 lrDistDecD1:=ABS((1/lrRadius)*((1*lrDistDecX)+(1*lrDistDecY)));
42 lrDistAccD2:=ABS((1/lrRadius)*((1*lrDistAccX)+(-1*lrDistAccY)));
43 lrDistDecD2:=ABS((1/lrRadius)*((1*lrDistDecX)+(-1*lrDistDecY)));
44
45 // Determination of Rotational Acceleration and Deceleration/s²
46 DynAxis1.lAcceleration:=2*lrDistAccD1/(lrTpsAcc*lrTpsAcc);
47 DynAxis1.lDeceleration:=2*lrDistDecD1/(lrTpsDec*lrTpsDec);
48 DynAxis2.lAcceleration:=2*lrDistAccD2/(lrTpsAcc*lrTpsAcc);
49 DynAxis2.lDeceleration:=2*lrDistDecD2/(lrTpsDec*lrTpsDec);
50
51 // Determination of velocity, rev/s
52 DynAxis1.lVelocity:=DynAxis1.lAcceleration*lrTpsAcc;
53 DynAxis2.lVelocity:=DynAxis2.lAcceleration*lrTpsAcc;

```